

DATASHEET

GS130 / GS230 SUPERCAPACITOR

Revision 4.5, May 2020

Electrical Specifications

The GS130 is a single cell supercapacitor. The GS230 is a dual cell supercapacitor with two GS130 cells in series, so GS230 capacitance = Capacitance of GS130/2 and GS230 ESR = 2 x GS130 ESR.

Table 1: Absolute Maximum Ratings

Parameter	Name		Conditions	Min	Typical	Max	Units
Terminal Voltage	V _{peak}	GS130		0		2.75	V
		GS230				5.5	
Temperature	T _{max}			-40		+70	°C

Table 2: Electrical Characteristics

Parameter	Name		Conditions	Min	Typical	Max	Units
Terminal Voltage	V _n	GS130		0		2.5	V
		GS230		0		5.0	
Capacitance	C	GS130	DC, 23°C	1920	2400	2880	mF
		GS230		960	1200	1440	
ESR	ESR	GS130	DC, 23°C		15	18	mΩ
		GS230			25	30	
Leakage Current	I _L		2.3V, 23°C 120hrs		2.5	5	μA
RMS Current	I _{RMS}		23°C			8	A
Peak Current ¹	I _P		23°C			30	A

¹Non-repetitive current, single pulse to discharge fully charged supercapacitor.

Table 3: Thickness

GS130F	1.9mm	No adhesive tape on underside of the supercapacitor	GS130G	2.0mm	Adhesive tape on underside, release tape removed
GS230F	3.9mm		GS230G	4.0mm	

This datasheet should be read in conjunction with the [CAP-XX Supercapacitor Product Guide](#) which contains information common to our product lines.

Definition of Terms

In its simplest form, the Equivalent Series Resistance (ESR) of a capacitor is the real part of the complex impedance. In the time domain, it can be found by applying a step discharge current to a charged cell as in Fig. 1. In this figure, the supercapacitor is pre-charged and then discharged with a current pulse, $I = 1A$ for duration 0.01 sec.

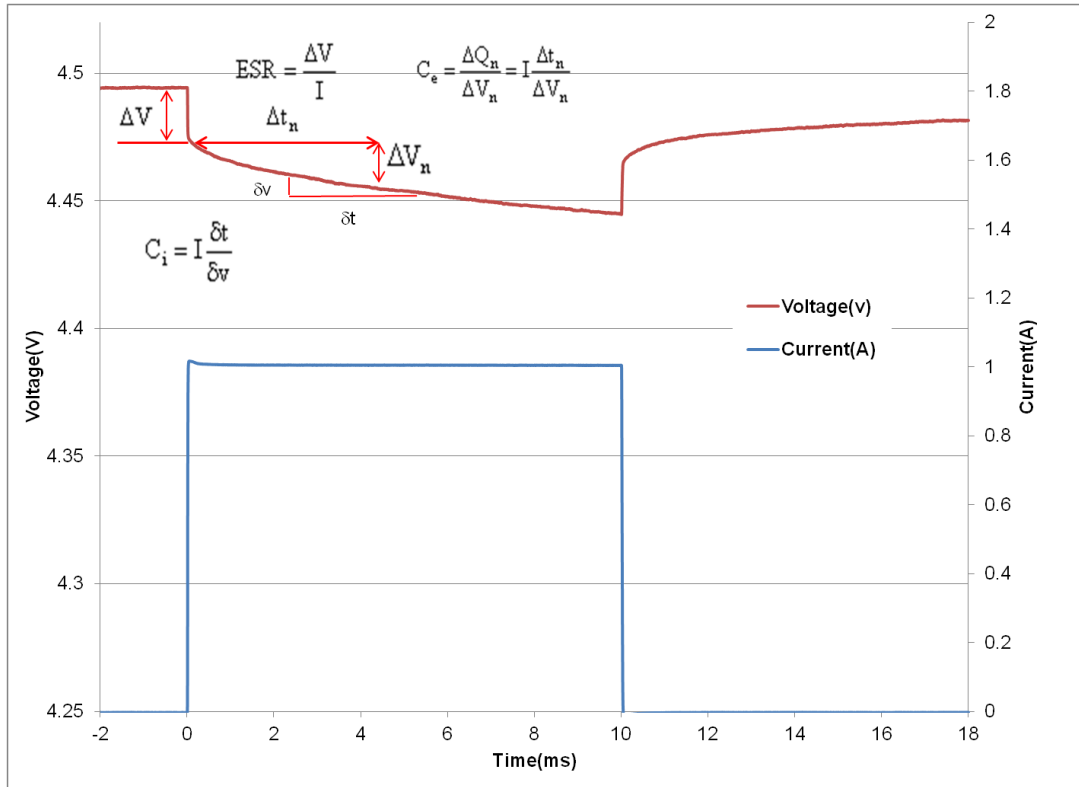


Figure 1: Effective capacitance, instantaneous capacitance and ESR for a GS230

The ESR is found by dividing the instantaneous voltage step (ΔV) by I . In this example $= (4.49V - 4.475V)/1A = 15m\Omega$.

The instantaneous capacitance (C_i) can be found by taking the inverse of the derivative of the voltage, and multiplying it by I .

The effective capacitance for a pulse of duration Δt_n , $C_e(\Delta t_n)$ is found by dividing the total charge removed from the capacitor (ΔQ_n) by the voltage lost by the capacitor (ΔV_n). For constant current $C_e(\Delta t_n) = I \times \Delta t_n / \Delta V_n$. C_e increases as the pulse width increases and tends to the DC capacitance value as the pulse width becomes very long (~10 secs). After 2msecs, Fig 1 shows the voltage drop $V_{2ms} = (4.475V - 4.461V) = 14mV$. Therefore $C_e(2ms) = 1A \times 2ms / 14mV = 142mF$. After 10ms, the voltage drop $= 4.475V - 4.445V = 30mV$. Therefore $C_e(10ms) = 1A \times 10ms / 30mV = 333mF$. The DC capacitance of a GS230 = 1.2 F. Note that ΔV , or IR drop, is not included because very little charge is removed from the capacitor during this time. C_e shows the time response of the capacitor and it is useful for predicting circuit behaviour in pulsed applications.

Measurement of DC Capacitance

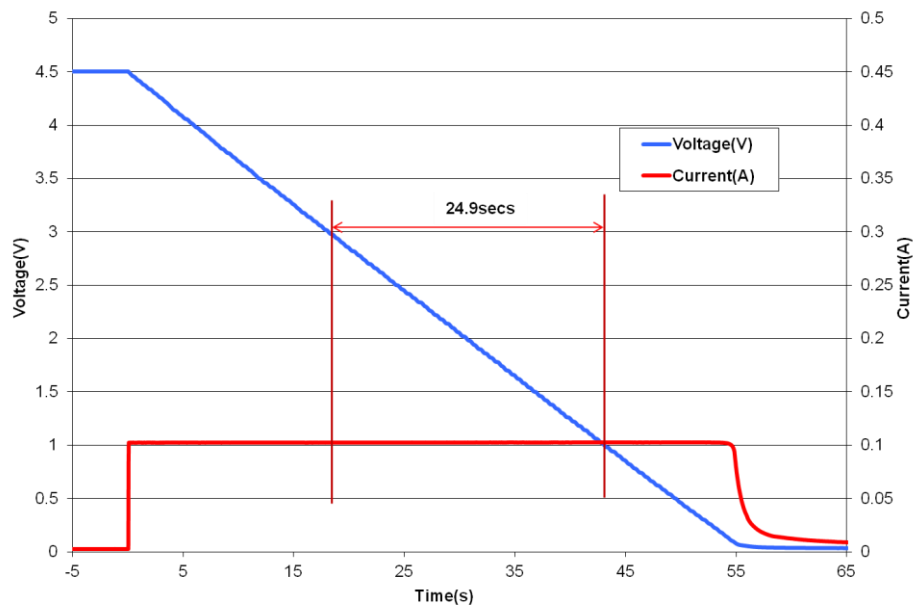


Fig 2: Measurement of DC Capacitance for a GS230

Fig 2 shows the measurement of DC capacitance by drawing a constant 100mA current from a fully charged supercapacitor and measuring the time taken to discharge from 1.5V to 0.5V for a single cell, or from 3V to 1V for a dual cell supercapacitor. In this case, $C = 0.1A \times 24.9s / 2V = 1245mF$, which is well within the 1200mF +/- 20% tolerance for a GS230 cell.

Measurement of ESR

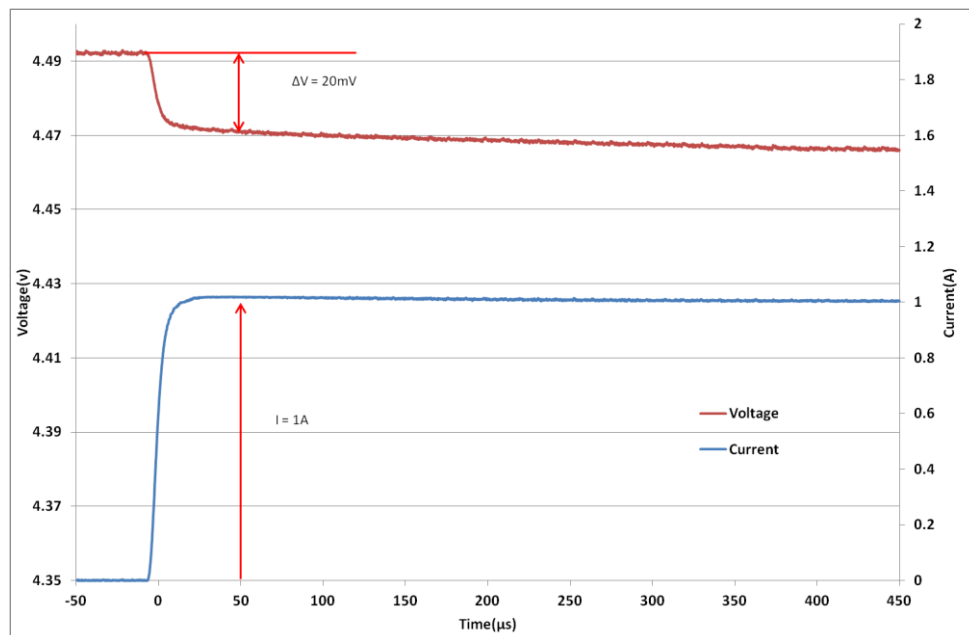


Fig 3: Measurement of ESR for a GS230

Fig 3 shows DC measurement of ESR by applying a step load current to the supercapacitor and measuring the resulting voltage drop. CAP-XX waits for a delay of 50μs after the step current is applied to ensure the voltage and current have settled. In this case the ESR is measured as $20mV/1A = 20m\Omega$.

Effective Capacitance (Ceff)

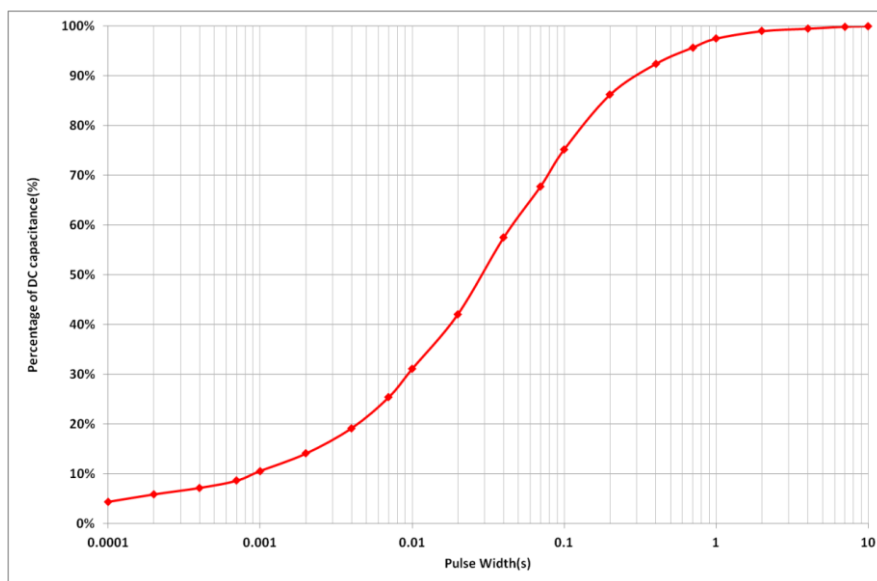


Fig 4: Effective Capacitance

Fig 4 shows the effective capacitance for the GS130, GS230 @ 23°C. This shows that for a 1ms PW, you will measure 10% of DC capacitance or 240mF for a GS130 or 120mF for a GS230. At 10ms, you will measure 31% of the DC capacitance, and at 100ms you will measure 72% of DC capacitance. Ceffective is a time domain representation of the supercapacitor's frequency response. If, for example, you were calculating the voltage drop if the supercapacitor was supporting 1A for 10ms, then you would use the $C_{eff}(10\text{msecs}) = 31\%$ of DC capacitance = 372mF for a GS230, so $V_{drop} = 1\text{A} \times \text{ESR} + 1\text{A} \times \text{duration}/C = 1\text{A} \times 25\text{m}\Omega + 1\text{A} \times 10\text{ms} / 372\text{mF} = 52\text{mV}$. The next section on pulse response shows how the effective capacitance is sufficient for even short pulse widths.

Pulse Response

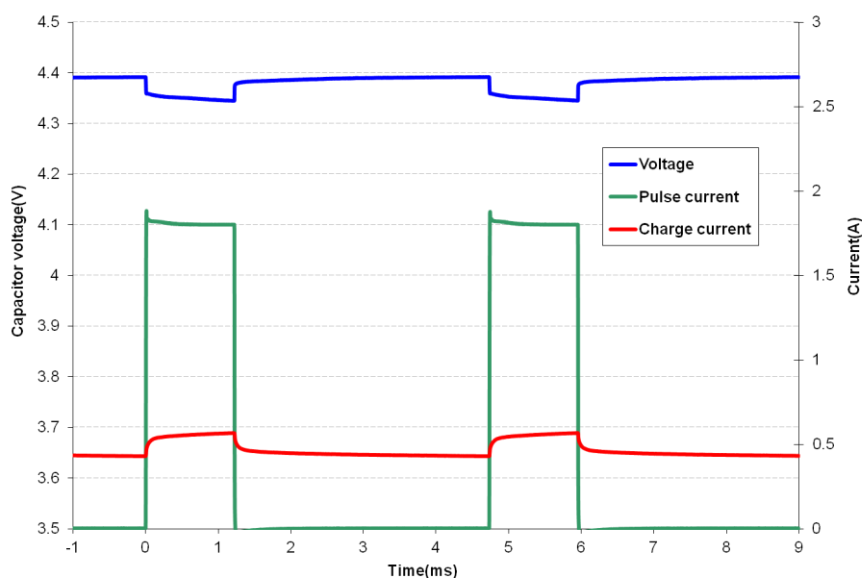


Fig 5 shows that the GS230 supercapacitor does an excellent job supporting a GPRS class 10 pulse train, drawing 1.8A for 1.1ms at 25% duty cycle. The source is current limited to 0.6A and the supercapacitor provides the 1.2A difference to achieve the peak current. At first glance the freq response of Fig 8 indicates the supercapacitor would not support a 1.1ms pulse, but the Ceff of 132mF coupled with the low ESR supports this pulse train with only ~45mV droop in the supply rail.

Fig 5: GS230 Pulse Response with GPRS Class 10 Pulse Train

Accurate Calculation of Voltage Drop for a Pulse Using Ceff

The combination of the method used by CAP-XX to measure ESR and effective capacitance for a given pulsewidth given in Fig 4 enable the accurate calculation of voltage drop for a pulse with current I and pulsewidth T as $V_{drop} = I \cdot [ESR + T/C_{eff}(T)]$. Using the pulse train of Fig 5 as an example, $I = 1.8A - 0.6A = 1.2A$. $T = 1.1ms$. Nominal DC capacitance = 1200mF, and from Fig 4, $C_{eff}(1.1ms) = 12\% \times 1200mF = 144mF$. Nominal ESR = 24mΩ, so $V_{drop} = 1.2A[0.024\Omega + 0.0011s/0.144F] = 38mV$. Fig 5 shows a voltage drop = 45mV verifying that the calculation is a good approximation. This avoids the need to run SPICE for a simple calculation.

DC Capacitance variation with temperature

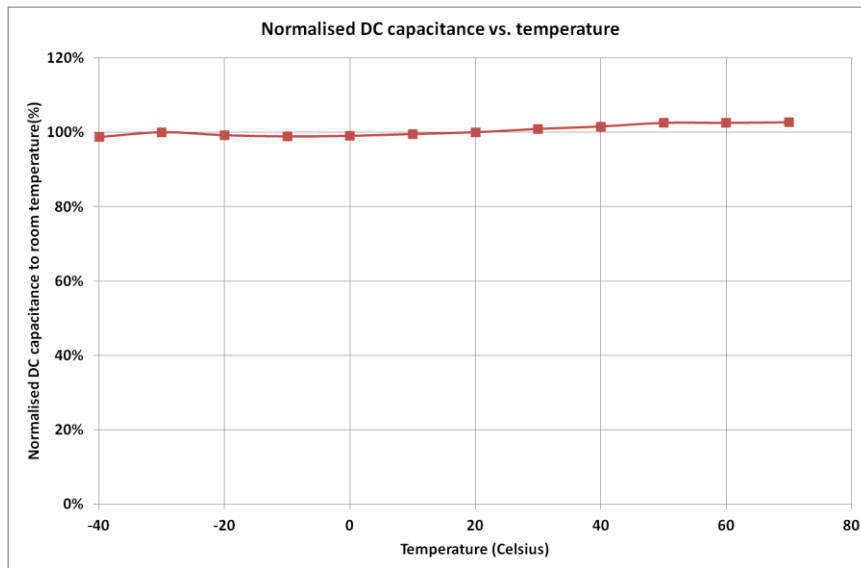


Fig 6: Capacitance change with temperature

Fig 6 shows that DC capacitance is approximately constant with temperature.

ESR variation with temperature

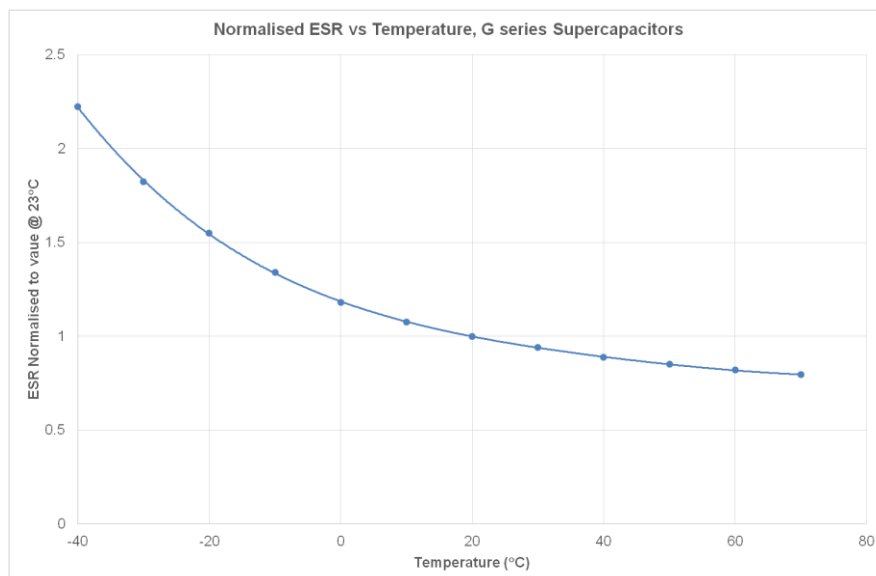


Fig 7: ESR change with temperature

Fig 7 shows that ESR at -40°C is ~2.2 x ESR at room temp, and that ESR at 70°C is ~0.8 x ESR at room temperature.

Frequency Response

GS230 Magnitude and Phase vs. Frequency

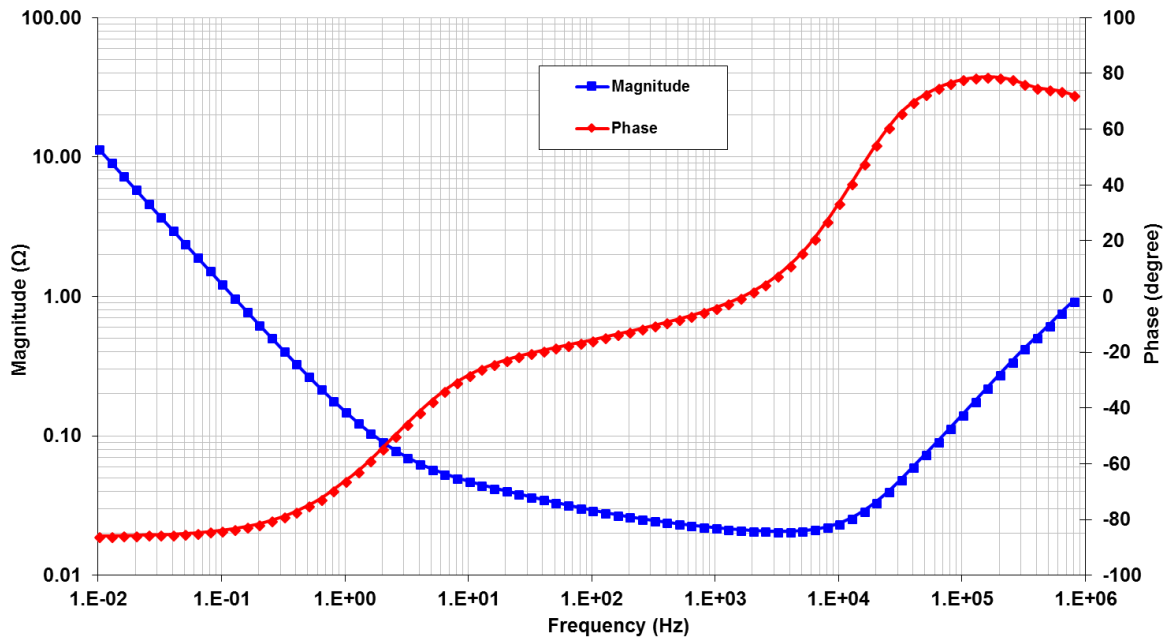


Fig 8: Frequency Response of Impedance (biased at 5V with a 50mV test signal)

GS230 ESR, Capacitance and Inductance vs. Frequency

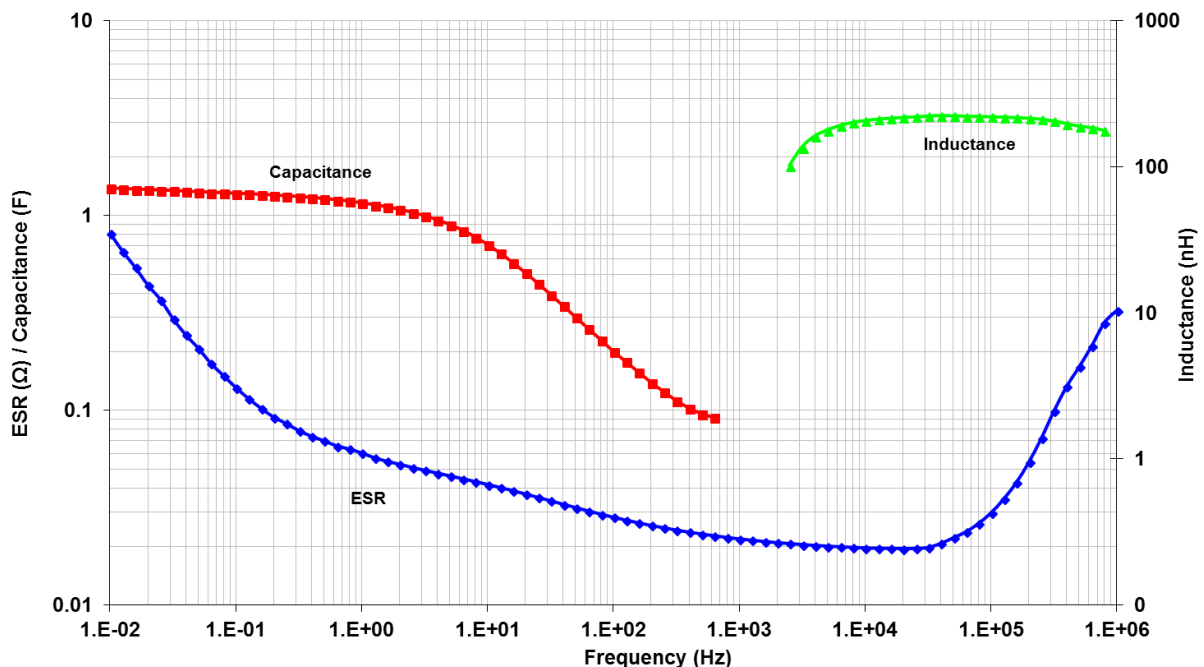


Fig 9: Frequency Response of ESR, Capacitance & Inductance

Fig 8 shows the supercapacitor behaves as an ideal capacitor until approx 3 Hz when the magnitude no longer rolls off proportionally to $1/\text{freq}$ and the phase crosses -45° . Performance of supercapacitors with frequency is complex and the best predictor of performance is Fig 4 showing effective capacitance as a function of pulsewidth.

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Leakage Current

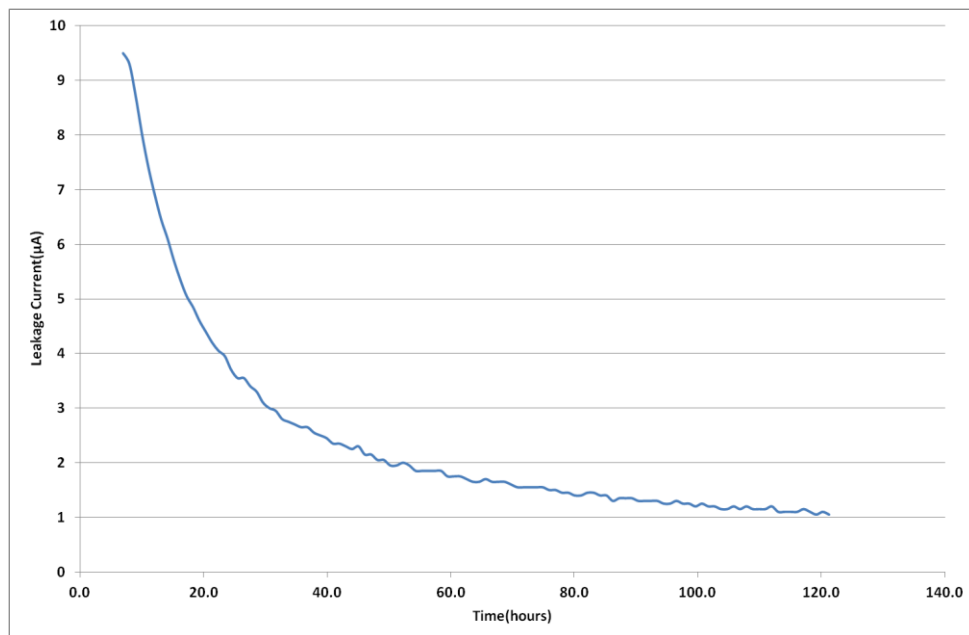


Fig 10: Leakage Current

Fig 10 shows the leakage current for GS130 at room temperature. The leakage current decays over time, and the equilibrium value leakage current will be reached after ~120hrs at room temperature. The typical equilibrium leakage current is ~1µA at room temperature. At 70°C leakage current will be ~10µA.

Charge Current

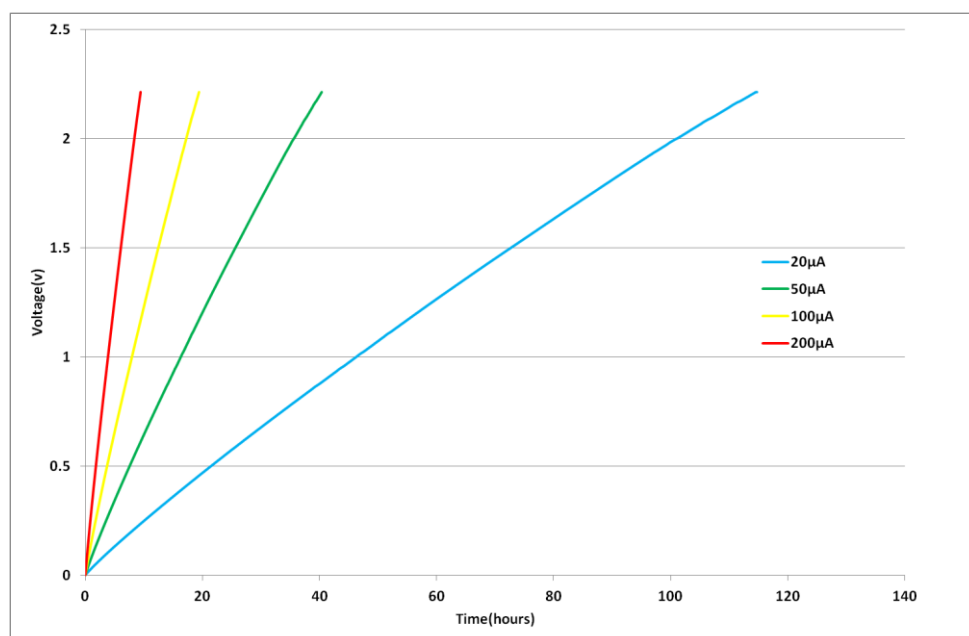
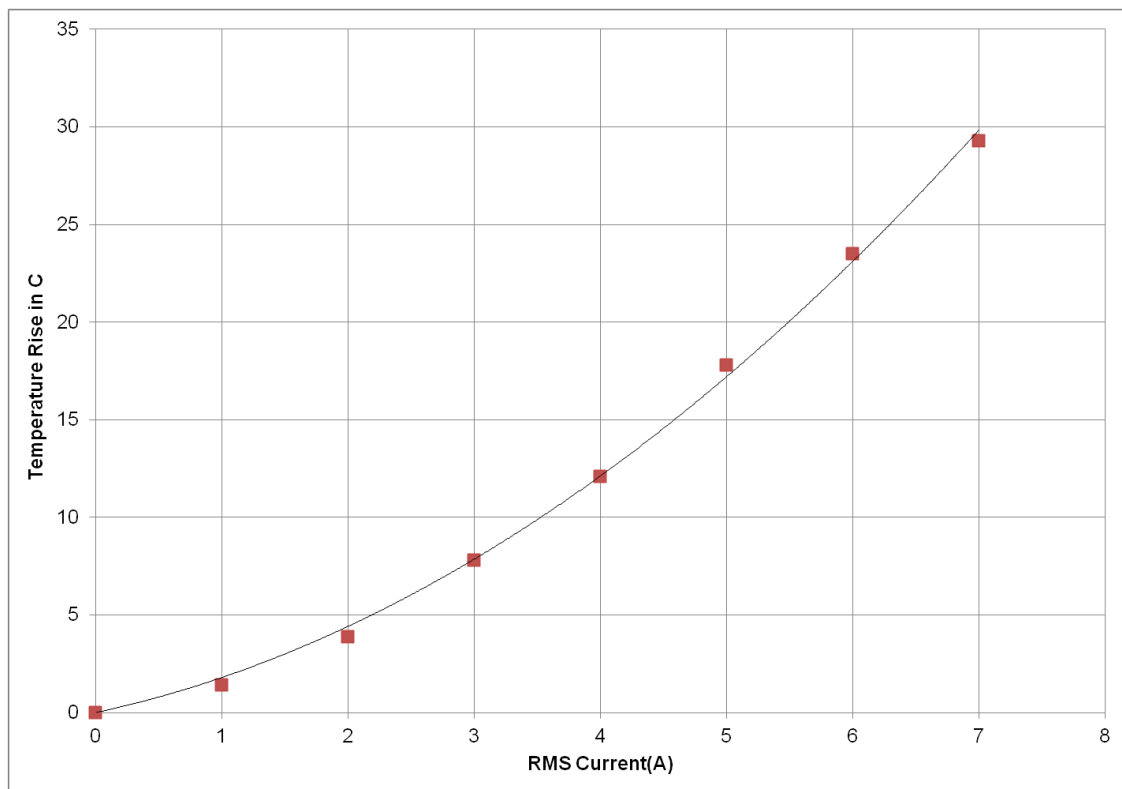


Fig 11: Charging a GS130 with low current

The corollary to the slow decay in leakage currents shown in Fig 10 is that charging a supercapacitor at very low currents takes longer than theory predicts. At higher charge currents, the charge rate is as theory predicts. For example, it should take $2.4\text{F} \times 2.2\text{V} / 0.00002\text{A} = 80\text{hrs}$ to charge a 2.4 F supercapacitor to 2.2V at 20µA, but Fig 11 shows it took 115hrs. At 100µA charging occurs at a rate close to the theoretical rate.

RMS Current**Fig 12: Temperature rise in GS230 with RMS current**

Continuous current flow into/out of the supercap will cause self heating, which limits the maximum continuous current the supercapacitor can handle. This is measured by a current square wave with 50% duty cycle, charging the supercapacitor to rated voltage at a constant current, then discharging the supercapacitor to half rated voltage at the same constant current value. For a square wave with 50% duty cycle, the RMS current is the same as the current amplitude. Fig 12 shows the increase in temperature as a function of RMS current. From this, the maximum RMS current in an application can be calculated, for example, if the ambient temperature is 40°C, and the maximum desired temperature for the supercapacitor is 70°C, then the maximum RMS current should be limited to 7A, which causes a 30°C temperature increase.

CAP-XX Supercapacitors Product Guide

Refer to the package drawings in the [CAP-XX Supercapacitors Product Guide](#) for detailed information of the product's dimensions, PCB landing placements, active areas and electrical connections, as well for information on endurance and shelf life, transportation and storage, assembly and soldering, safety and RoHS/REACH certification.